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Makeup Mirror Heliostat

Section 27096, Group 12

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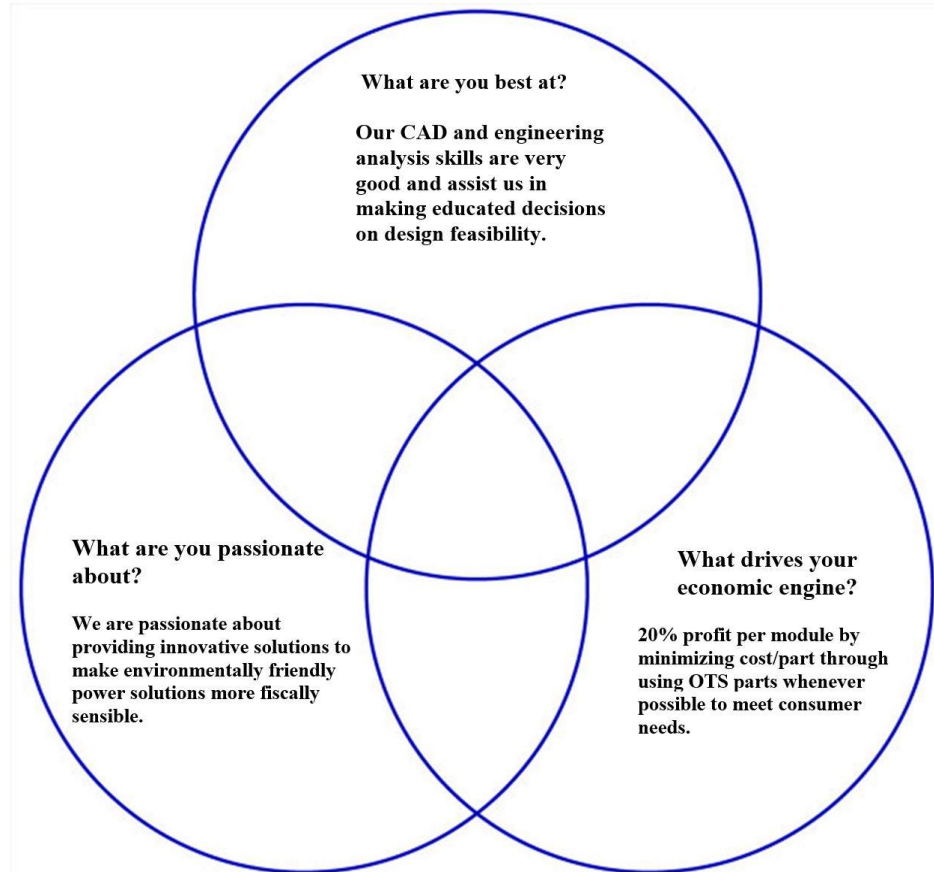
Presentation Outline

- Hedgehog Concept
- Product Overview
- Subsystem Identification
- Subsystem Descriptions
- Subsystem Analyses
- Key Features
- Cost Breakdown
- Technology Readiness Level
- Summary/Conclusion

Hedgehog Concept:

To use our CAD and engineering analysis skills to make heliostat fields more fiscally sensible and meet consumer needs by minimizing cost and maintaining quality.

Hedgehog Concept



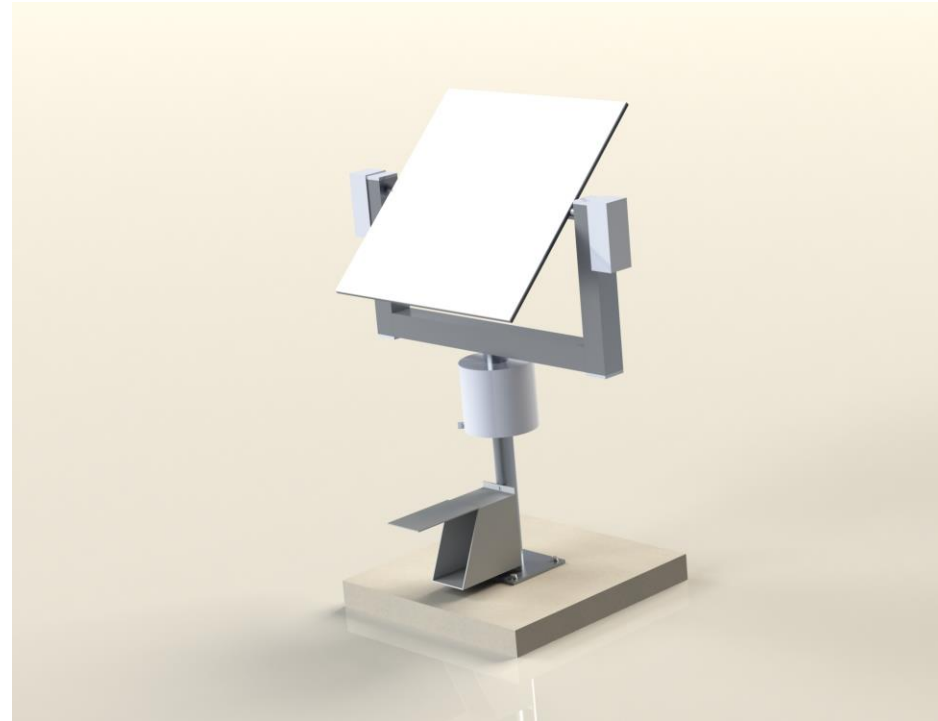
Product Overview

Objectives:

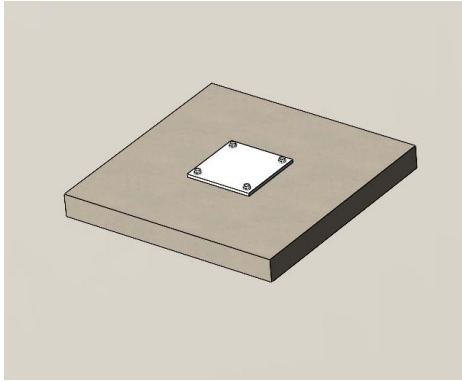
- Design a small-scale low-cost heliostat
- Maximize thermal efficiency
- Automated sun-tracking control

Overall dimensions:

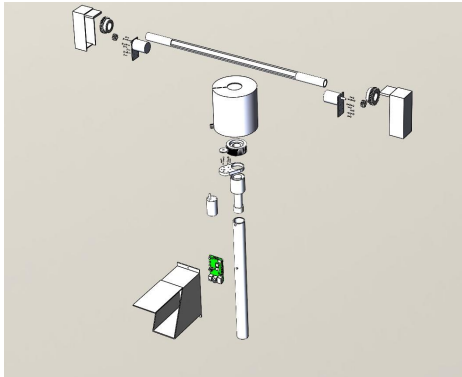
- 4 heliostats per module
- 360° rotation along two axes
- Max. size: 0.5 m × 0.73 m × 1.07 m
- Total mass: 33.6 kg



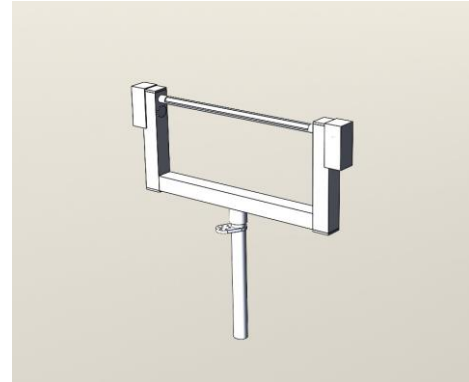
Subsystem Identification



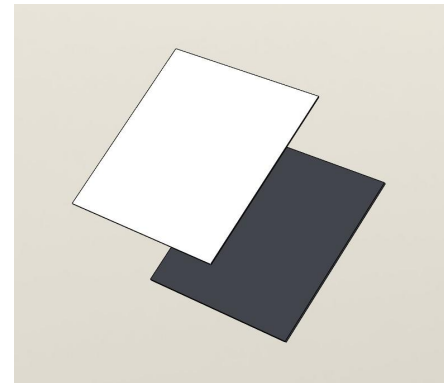
Foundation



Sun-tracking Mechanics



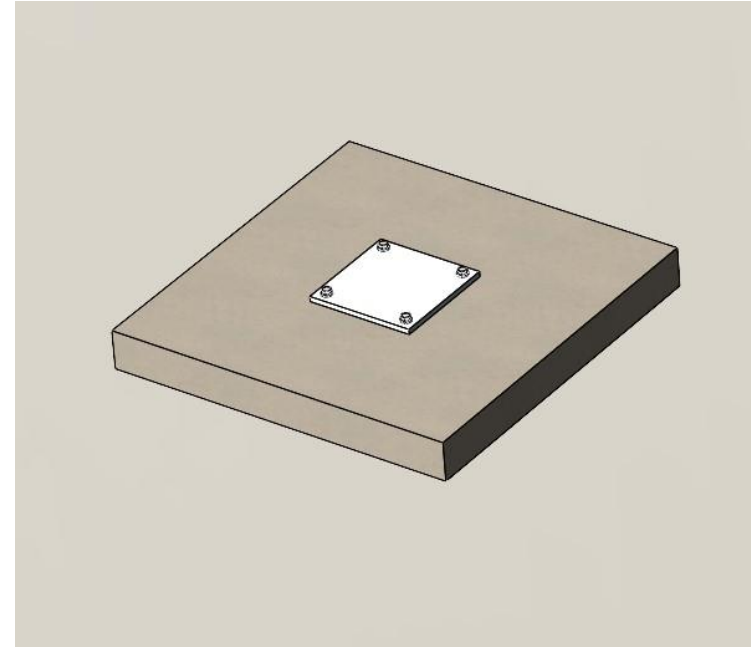
Support



Reflective Surface

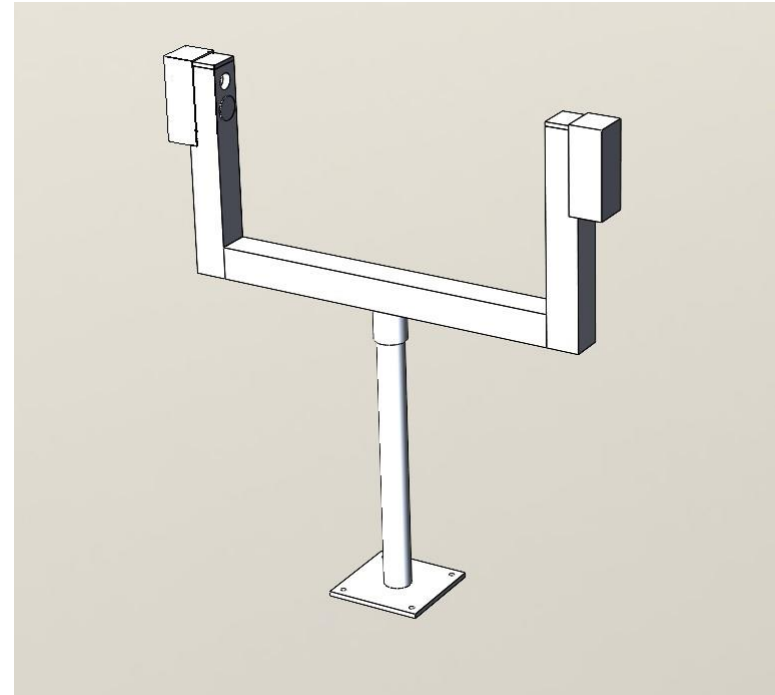
Foundation

- The concept chosen for the foundation was a plated concrete block.
- The plate is made of aluminum while the screws are made of zinc-plated-steel.
- This concept delivers good weight and stability to the system for a relatively low cost.
- It also resists corrosion from the ambient weather in Las Vegas, NV.
- This design benefits from low manufacturing cost and high manufacturability.



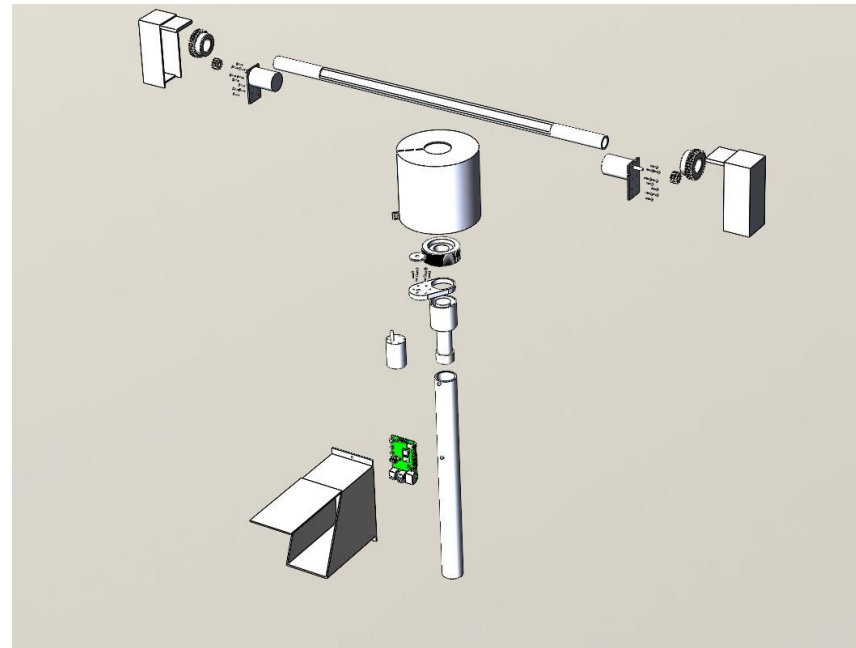
Support

- The concept chosen for the support was the 'Makeup Mirror'.
- The entire support system is made of either square or round aluminum tubing, ensuring corrosion resistance.
- The support rod is made of aluminum as well.
- The support and the sun-tracking-mechanics designs blend to avoid extra material cost.
- Worst case scenarios were simulated to achieve a factor of safety of well over $N=2$.



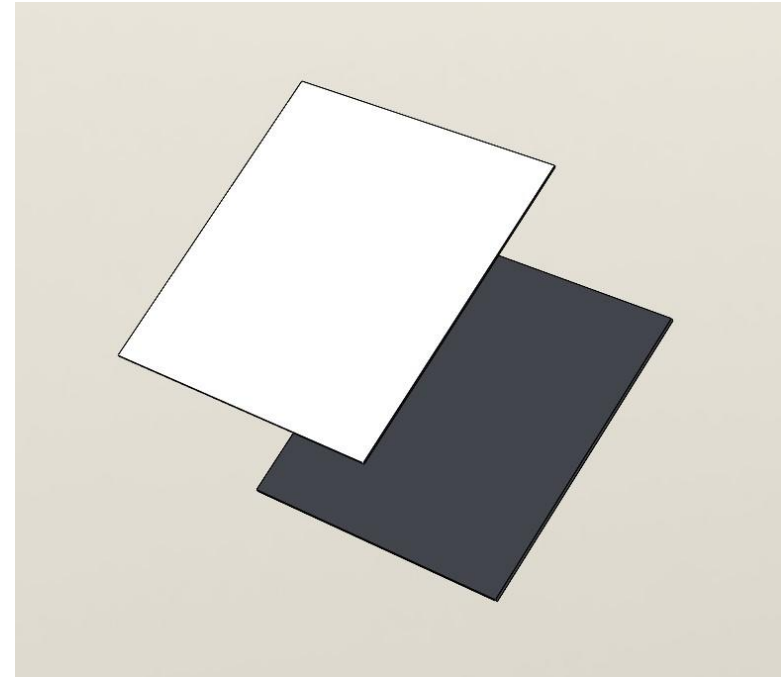
Sun-tracking Mechanics

- Raspberry PI 4 Pico
- Two 24V DC motors allow the mirror to rotate vertically
- A system of two gears inside an aluminum casing provides azimuthal rotation
- The gears are custom-made and 3D-printed using Thermoplastic-blend filament
- Closed-loop control



Reflective Surface

- Flat rectangular glass
- Silver coating for high reflectivity: 90%
- Area of each mirror is 0.25 m^2
- Aluminum frame adhesively attached to the reflective surface
 - Master Bond Supreme 10HT
- All parts are commercially available
- All components operate well under high temperatures



Design Subsystem Analyses

Foundation: Bolt Analysis

Objective: Avoid shear failure in bolt due to wind induced drag force.

Assumptions:

- $C_D = 1.17$
- $A_{refl} = 0.25m^2$
- $V_{wind} = 40.2 \frac{m}{s}$
- $A_{bolt} = 3.16 * 10^{-5} m^2$
- $USS_{bolt} = 0.75 * \sigma_{UTS} = 315MPa.$
- $H_{mirror} = 0.745m$
- $L_{pole\ to\ bolt} = 0.15m$

Calculations:

- $F_D = \frac{C_D A_{refl} V_{wind}^2}{2} = \frac{1.17 * 0.25 * 40.2^2}{2} = 236.346N.$
- $M_{base} = F_D * H_{mirror} = 236.346 * 0.745 = 176.077 Nm$
- $F_{bolts} = \frac{M_{base}}{L_{pole\ to\ bolt}} = \frac{176.077}{0.15} = 1173.8518 N$
- $F_{bolt} = \frac{F_{bolts}}{2} = \frac{1173.8518}{2} = 586.93 N$
- $\tau_{bolt} = \frac{F_D}{A_{bolt}} = \frac{586.93N}{3.16 * 10^{-5} m^2} = 18.574MPa < 315MPa.$

Design Subsystem Analyses

Support: Support beam failure

Objective: Avoid damage to the support beam from wind induced force.

Assumptions:

- $C_D = 1.17$
- $A_{refl} = 0.25m^2$
- $V_{wind} = 40.2 \frac{m}{s}$
- $A_{supp} = 0.589m^2$
- $\sigma_{UTS} = 276MPa$
- Entirety of drag force applied as bending stress to the support beam.
- $USS_{bolt} = 0.75 * \sigma_{UTS} = 315MPa.$
- $H_{mirror} = 0.745m$
- $L_{pole\ to\ polt} = 0.15m$
- $D = 0.0422m, y = .02108m$
- $I = 8.104 * 10^{-8}m^4$

Calculations:

- $F_D = \frac{C_D A_{refl} V_{wind}^2}{2} = \frac{1.17 * 0.25 * 40.2^2}{2} = 236.346N.$
- $M_{base} = F_D * H_{mirror} = 236.346 * 0.745 = 176.077 Nm$
- $\sigma_{supp} = \frac{M_{base} * y}{I} = \frac{176.078 * .02108N}{8.104 * 10^{-8}m^4} = 45.8MPa < 276MPa.$

Design Sub-system Analyses

Sun-tracking Mechanics: Shaft Failure

Objective: Ensure that the shaft does not fail under excess stress.

Assumptions:

- Shear failure – Tresca Criterion: $\tau_{max} = 0.5S_y$
- Yield strength of aluminum: 276 MPa
- Polar moment of inertia for hollow tube: $\frac{\pi(R_i^4 + R_o^4)}{2} = 5.3658 \cdot 10^{-8} m^4$
- Maximum torque provided by motors: 1.471 N-m

Calculations: the maximum shear stress at a radial distance $R_o = 25.4 mm$ and motor torque T is found as:

$$\tau = \frac{TR_o}{J} = 348.165 kPa$$

This results in a factory of safety of 396.



Design Sub-system Analyses

Reflective Surface: Solar Concentration Ratio

Objective: Provide a solar concentration ratio greater than 1000 suns

Assumptions:

- Optical loss $\eta_o = 0.4$
- Receiver area $A_r = 1 \text{ m}^2$
- Area of each reflective surface $A_{refl} = 0.25 \text{ m}^2$
- A heliostat field consisting of 1900 heliostat modules, resulting in $N_h = 7600$ heliostats

Calculations: the solar concentration ratio, c , was found as

$$c = (1 - \eta_o) \cdot \frac{A_{refl} N_h}{A_r} = 1140 \text{ suns}$$

Design Sub-system Analyses

Reflective Surface: Thermal Input Power

Objective: Provide a thermal input power of 1 MW after losses.

Assumptions:

- Incidence angle, θ , optimized to have a cosine value of 0.9-1.0
- Direct normal irradiance, G_{bn} , provided from:

<https://midcdmz.nrel.gov/apps/sitehome.pl?site=NPC>

Calculations: beam irradiance on a tilted surface is found as:

$$G_{bt} = G_{bn} \cos \theta$$

Therefore, the thermal input, \dot{Q} , can be expressed as follows:

$$\dot{Q} = (1 - \eta_o) \eta_{cos} G_{bn} A_{refl} N_h$$

For $G_{bn} \geq 1000 \text{ W/m}^2$, the thermal input is equal to 1.03 MW.

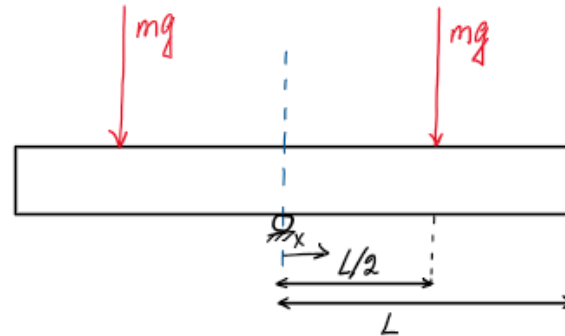
Design Sub-system Analyses

Reflective Surface: Aluminum Frame Failure

Objective: Ensure that the aluminum frame does not fail under bending

Assumptions:

- Frame modeled as a rectangular beam fixed at its center
- Maximum bending stress occurs at a slope angle $\beta = 0^\circ$
- Flexural strength of aluminum: 299 MPa



- Due to symmetry, one half of the beam can be considered for analysis

Design Sub-system Analyses

Reflective Surface: Aluminum Frame Failure

Calculations:

- Bending stress, $\sigma_{bend} = \frac{My}{I}$
- The loads are concentrated at a length $L/2 = 0.125 \text{ m}$, where L is half of the frame length
- The moment, M , is found as: $M = \frac{mgL}{2}$, where m the sum of the masses of the frame and the reflective surface, divided by two.
 - $m = \frac{1}{2}(m_{frame} + m_{glass}) = \frac{1}{2}(4.29 + 1.84) = 3.065 \text{ kg}$
- The moment of inertia, I , is equal to $5.3343 \cdot 10^{-9} \text{ m}^4$
- Distance y is equal to half of the frame's thickness
- Therefore, the maximum bending stress was equal to 2.24 MPa
 - The resulting factor of safety is 133.5

Key Features

Fully Aluminum Construction

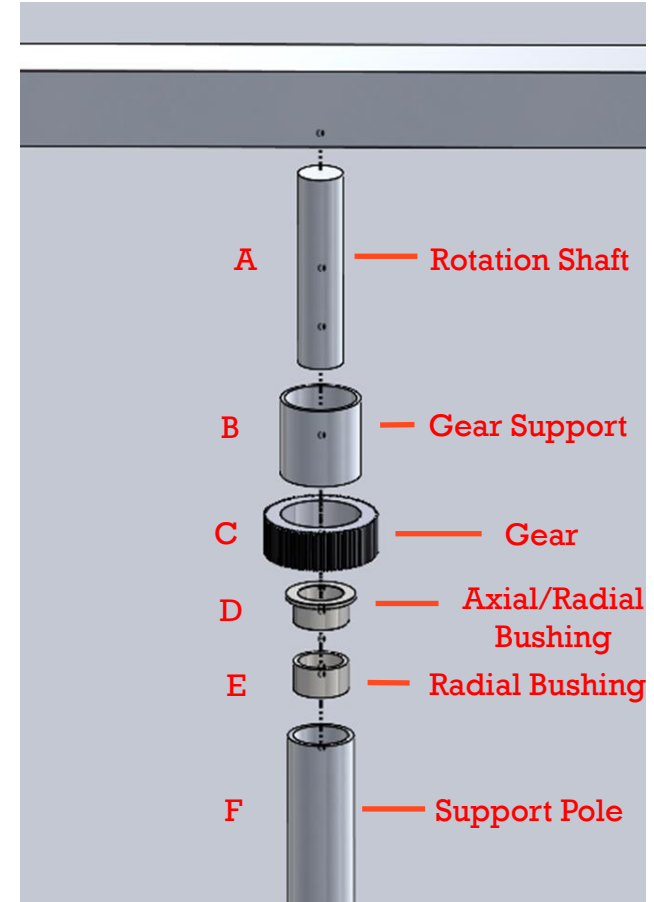
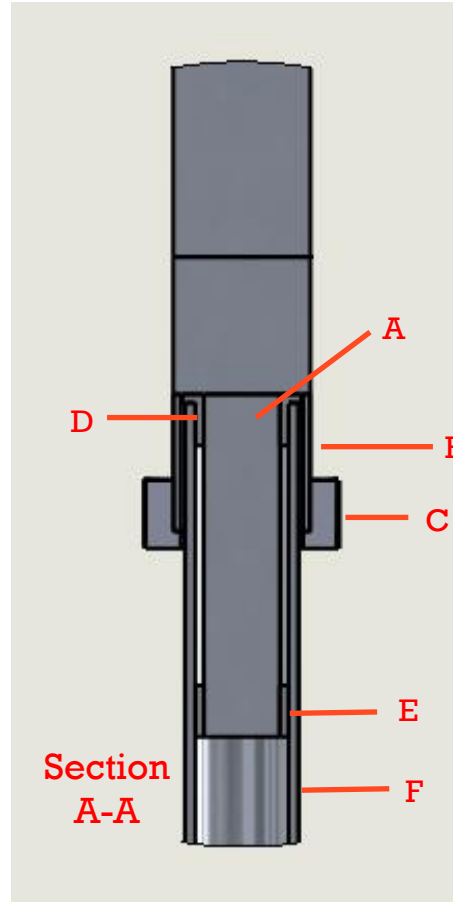
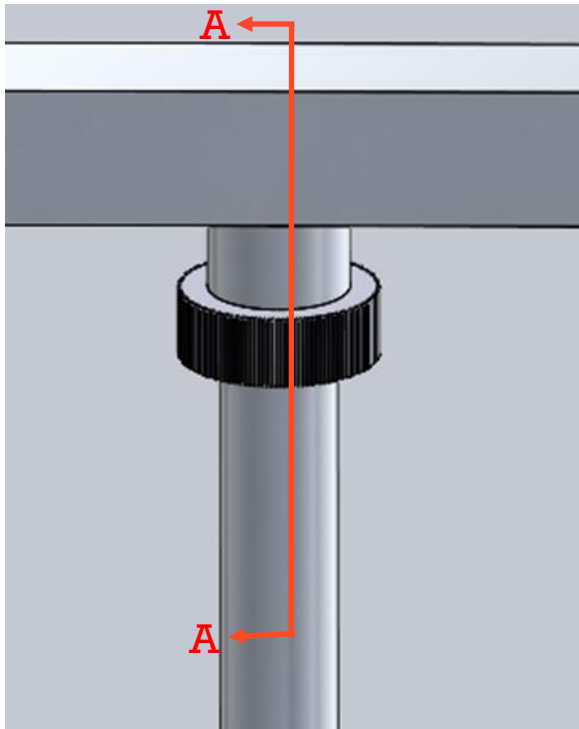
- Being constructed entirely of aluminum this heliostat has amazing strength and potential for longevity.
- The aluminum can easily be welded on site by a skilled welder making for a short assembly time.

360° Azimuthal and Elevation Rotation

- The “Makeup Mirror” design style allows for easy implementation of 360 degree azimuthal and elevation rotation.
- Unlimited rotation allows the heliostats to be placed in field without any consideration of aim caused by limited rotation.

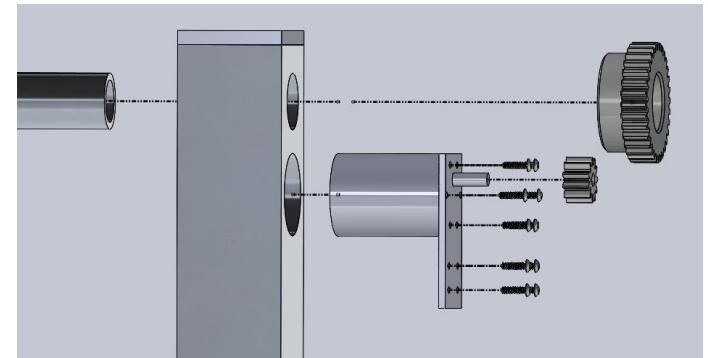
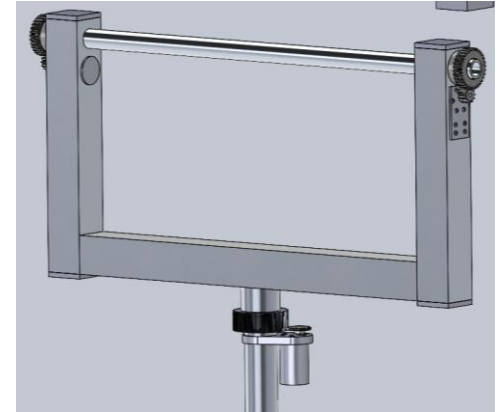
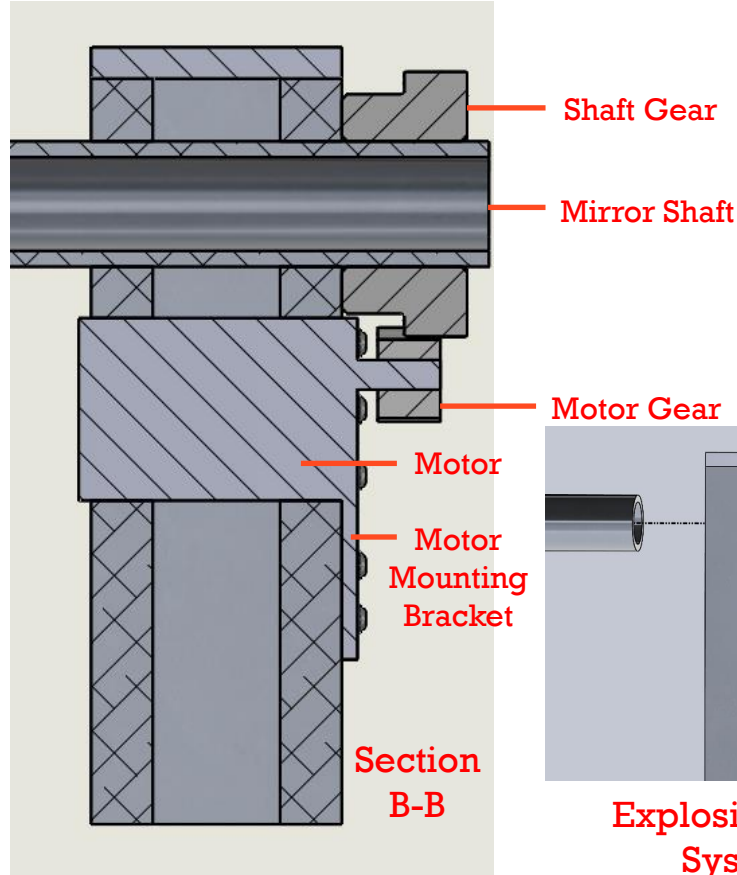
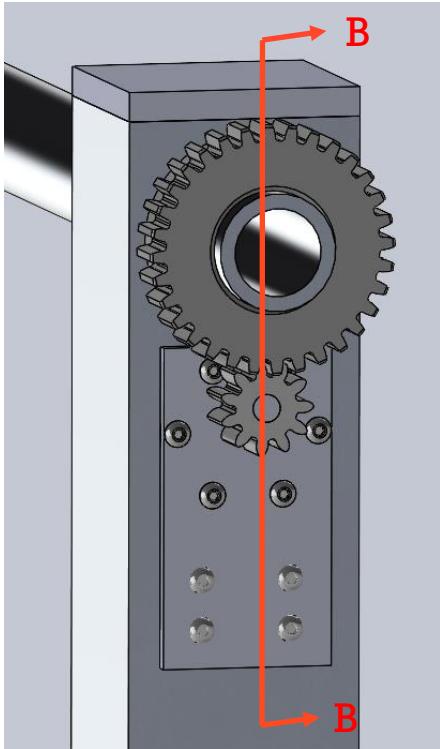
Key Features

Azimuthal Rotation



Key Features

Elevation Rotation



Explosion of Elevation Rotation System (one side only)

Cost \$\$\$

Raw Materials

- Aluminum, 3D Printing Filament, Concrete

OTS Parts

- Motors, Fasteners and Gears

Manufacturing Labor

- Custom Gears, Aluminum End Caps, Motor/Gear Housings, Shafts, Mirror, and Concrete Foundation

Expenses Breakdown:

Materials: \$373.82

OTS Parts: \$307.39

Manufacturing Labor: \$80

Assembly Labor: \$158

Energy Consumption: \$0

Total: \$919.21

Cost \$\$\$

Assembly Labor

- Welding at \$65/hour for about 2 hours
- Motor/gear/housing assembly at \$14/hour for about 2 hours

Energy Consumption

- No cost since power is supplied by the energy the heliostats generate.

Expenses Breakdown:

Materials: \$373.82

OTS Parts: \$307.39

Manufacturing Labor: \$80

Assembly Labor: \$158

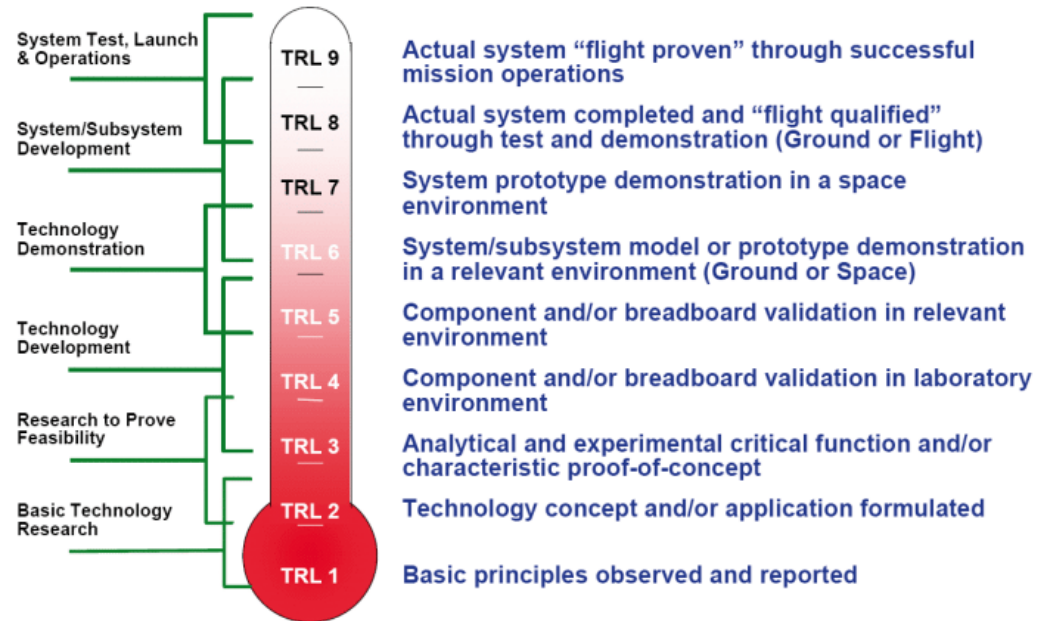
Energy Consumption: \$0

Total: \$919.21

Technology Readiness Level

Level 3

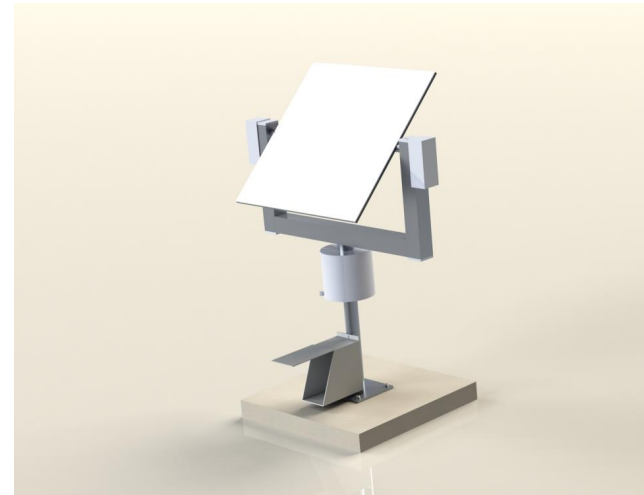
- The Makeup-Mirror heliostat is currently rated at a level 3.
- Upon further development and prototyping its level will increase



Summary

Makeup Mirror Heliostat

- Group 12 believes that the Makeup Mirror Heliostat should be chosen as a prototype for EML4502.
- This is due to:
 - Its innovative design combining a support subsystem and the sun-tracking mechanics subsystem.
 - Prototyping this system will allow for unique insight into the engineering design process.



Conclusion

- *Thank you* for attending our presentation!
- The Makeup Mirror Heliostat opens the door to sustainable, affordable power solutions and we are happy to take any questions.