## The Hive-Stat

## Small-Scale Modular Tracking Heliostat

## Group 13

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## Design Problem



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## Inspiration from Nature



Ease of Assembly- Straightforward assembly for a faster setup time

Optimized Field Placement- The design is optimized to deliver efficiency in a multitude of positions

## Ease of Assembly

Optimized Field Placement

Cost Reduction

Cost Reduction- Cost reduced by using more common materials and off the shelf parts

Department of Mechanical \& Aerospace Engineering


## Reflective Surface

- Hexagonal compact shape allows close tessellation of heliostats
- Shading effects eliminated by spacing heliostats close together so shadows do not reach reflective surface



## Reflective Surface Cont.

- Thermal Input Power, $\mathrm{N}=$ number of heliostats per module

$$
T I P=500 \cdot A_{\text {helio }} \cdot N=500 \cdot 0.1 \mathrm{~m}^{2} \cdot 6=300 \mathrm{~W}
$$

- Solar Concentration Ratio, assuming solar irradiance of $1000 \mathrm{~W} / \mathrm{m}^{2}$ and a collector area around the size of one heliostat

$$
S C R=\frac{2000}{N}=\frac{2000}{6}=333.33 \text { Suns }
$$

## Reflective Surface Cont.



$$
\begin{aligned}
& u(x, y)=\frac{P}{64 D a}\left(x^{3}-x^{2} a-3 x y^{2}-y^{2} a+\frac{4}{27} a^{3}\right)\left(\frac{4}{9} a^{2}-x^{2}-y^{2}\right) \\
& D=\frac{E t^{3}}{12\left(1-v^{2}\right)} \quad a=\frac{\sqrt{3}}{2} l \\
& u_{\max }=u(0,0)=\frac{P l^{4}\left(1-v^{2}\right)}{144 E t^{3}}=\frac{5.75 \times 0.48^{4}\left(1-0.22^{2}\right)}{144 \times 0.070 \times 0.002^{3}}=7.5 \mathrm{~mm}
\end{aligned}
$$

## Reflective Surface Cont.



$$
\begin{aligned}
& \alpha Q_{\text {sun }}-\varepsilon \sigma\left(T^{4}-T_{s k y}^{4}\right)-\mathrm{h}\left(T-T_{\text {air }}\right)=M C_{p} \frac{d T}{d t} \\
& \alpha=\frac{1}{Q_{\text {sun }}}\left[M C_{p} \frac{d T}{d t}+\varepsilon \sigma\left(T^{4}-T_{s k y}^{4}\right)\right] \\
& Q_{\text {sun }} \alpha=\varepsilon \sigma\left(T^{4}-T_{s k y}^{4}\right)-\mathrm{h}\left(T-T_{\text {air }}\right)
\end{aligned}
$$


$7.62\left[\frac{k W}{m^{2}}\right] \times 0.09=0.03 \times\left(5.67 \times 10^{-8}\right)\left[\frac{W}{m^{2} K^{4}}\right] \times\left(T^{4}-300^{4}\right)[K]+2\left[\frac{W}{m^{2} K}\right] \times(T-313.15)[K]$

$$
T=285.49^{\circ} \mathrm{C}
$$

## Structure

$\mathrm{q}=1 / 2 \rho \mathrm{v}^{2}$

$$
\begin{aligned}
& \mathrm{v}=12.38 \mathrm{~m} / \mathrm{s} \\
& \rho=1.225 \mathrm{~kg} / \mathrm{m}^{3} \\
& \mathrm{q}=93.874 \mathrm{~N} / \mathrm{m}^{2}
\end{aligned}
$$

$F=q A$

$$
\begin{aligned}
& \mathrm{A}=0.6 \mathrm{~m}^{\wedge} 2 \\
& \mathrm{q}=93.874 \mathrm{~N} / \mathrm{m}^{2} \\
& \mathrm{~F}=56.325 \mathrm{~N}
\end{aligned}
$$

$M$ max $=F r$
$\mathrm{F}=56.325 \mathrm{~N}$
$\mathrm{r}=609.6 \mathrm{~mm}$
$\mathrm{M}_{\text {max }}=34.335 \mathrm{~N}-\mathrm{M}$

$$
\begin{array}{ll}
I=\left(a_{1}{ }^{4} / 12\right) & a_{1}=13.54 \mathrm{in}^{2} \\
& I=2,800.872 \mathrm{in}^{4}
\end{array}
$$

$$
\begin{aligned}
& \mathrm{Mmax}=34.335 \mathrm{~N}-\mathrm{M} \\
& \mathrm{y}=6.77 \mathrm{in}^{2} \\
& \mathrm{I}=2,800.872 \mathrm{in}^{4} \\
& \sigma_{\max }=82.99 \mathrm{kPa}
\end{aligned}
$$

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## Structure Cont.

| Item | $\quad$ Weicht |
| :--- | :--- |
| Mirroor + mirror body | $16 \mathrm{lbs} \quad 4.28 \mathrm{lbs}$ |
| Hinge + pole + shaft |  |

Using Shigley's $8^{\text {th }}$ Ed. Shaft Bending Stress Eq. 7.3, assuming a well-rounded shaft for stress concentration:

$$
\sigma=K_{p} \frac{32 M_{a}}{\pi d^{3}}=1.7 \frac{32(2 * 10 \mathrm{lbs} * 2 ")}{\pi * 1^{3}}=1732 p s i
$$

Assuming a shear stress for 6061 aluminum as 30000 psi and a fatigue strength of 14000 psi for 500 million cycles, the factor of safety for near infinite life is about 8 and for peak loads about 17 .


## Controls Hardware cont.



-Bidirectional control for two brushed DC motor (DC 4V to 16V).
-Control one unipolar/bipolar stepper motor. -Maximum Motor Current: 3A continuous per channel, 5A peak.
-Buck-boost regulator to produce 5 V output (200mA max).

| Microcontroller | ATmega328P |
| :--- | :--- |
| Operating Voltage | 5 V |
| Input Voltage (recommended) | $7-12 \mathrm{~V}$ |
| Input Voltage (limit) | $6-20 \mathrm{~V}$ |
| Digital I/O Pins | 14 |
| PWM Digital I/O Pins | 6 |
| Analog Input Pins | 6 |
| DC Current per I/O Pin | 20 mA |
| DC Current for 3.3V Pin | 50 mA |
| Flash Memory | 32 KB |
| SRAM | 2 KB |
| EEPROM | 1 KB |
| Clock Speed | 16 MHz |



## Controls Hardware cont.

PRODUCT PARAMETERS


- With a speed of $10 \mathrm{~mm} / \mathrm{s}$, it would take about 35 seconds for the actuator to fully extend
- The actuator is more than fast enough to track the Sun as it travels
- Max power draw of 36 W for the actuator; 12.8 V battery with 10 aH
- Allows for 2 hours of full load continuous operation and 9 hours of low load continuous operation with a 20\% reserve capacity



## Actuation

- Angle control using two linear actuators
- Actuators each have two 2-axis joints for independent movement
- Reduced risk of damage to mirror in case of malfunction


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## Actuation Cont.

- Heliostats to be installed near Las Vegas, Nevada at $36.1699^{\circ} \mathrm{N}$
- Earth's tilt of $23.5^{\circ}$ gives a range of solar angles of $36.1699 \pm 23.5^{\circ}=59.67^{\circ}$ to $12.67^{\circ}$ from vertical in the South
- The Sun also moves $180^{\circ}$ from East to West, but most energy is available when the Sun is high in the sky, making angles near the horizon less desirable to reach



## Actuation Cont.

Assumption: Tower and heliostat field is North-South aligned with the tower in the South to minimize Sun-tower angle

Assumption: Heliostats are located between 50 and 100 meters from the tower

$$
\begin{aligned}
& \theta_{\min }=\tan ^{-1} \frac{100 m}{50 m}=63.43^{\circ} \text { above horizon }=26.57^{\circ} \text { from vertical } \\
& \theta_{\max }=\tan ^{-1} \frac{50 m}{50 m}=45^{\circ} \text { above horizon }=45^{\circ} \text { from vertical }
\end{aligned}
$$

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Actuation Cont.

- Heliostat works by reflecting light, so the Law of Reflection is used
- Angle of Incidence = Angle of Reflection
- Heliostat normal bisects angle between Sun and tower


## Actuation Cont.

- Maximum heliostat angle North-South from vertical

$$
\begin{aligned}
& \text { Max }=\max \left(\text { solar angle }-\frac{a b s(\text { Tower angle }- \text { solar angle })}{2}\right. \\
& =59.67-\frac{59.67-45}{2}=52.34^{\circ} \text { from vertical towards South }
\end{aligned}
$$

- Minimum heliostat angle North-South from vertical

$$
\begin{aligned}
& \text { Min }=\min \left(\frac{\text { abs }(\text { Tower angle }- \text { solar angle })}{2}+\text { solar angle }\right) \\
& =\frac{26.57-12.67}{2}+12.67=19.62^{\circ} \text { from vertical towards South }
\end{aligned}
$$

## Actuation Cont.

- Maximum heliostat angle East-West from vertical
- Sun reaches fully West and fully East, $90^{\circ}$ from tower in each direction

$$
\text { Min }=\operatorname{Max}=\frac{90+0}{2}=45^{\circ} \text { from vertical in both directions }
$$

Actuation Cont.


- North-South angle achieved by actuator mounted high on pillar, lowest angle needed is $0^{\circ}$ for neutral position in storms
- East-West angle controlled by lower-mounted actuator for equal control in either direction
- Attached to plastic support by clips screwed onto connector

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## Ground mounting



## Ground Mounting Cont.

## Parallel Axis Theorem

$$
\begin{gathered}
I=4\left(\frac{\pi d^{4}}{64}+\frac{\pi d^{2}}{4} L^{2}\right) \\
I=4\left(\frac{\pi(0.032 m)^{4}}{64}+\frac{\pi(0.032 m)^{2}}{4} 0.1299^{2}\right)=0.209 \mathrm{~m}^{4}
\end{gathered}
$$

Failure Mode

$$
\begin{gathered}
\sigma_{\max }=\frac{y M_{\max }}{I} \\
\sigma_{\max }=\frac{(0.1299 \mathrm{~m})(23.45 \mathrm{Nm})}{0.209 \mathrm{~m}^{4}}=14.57
\end{gathered}
$$

## Cost Table Summary



## Total Cost: \$373.75

*Retail pricing for prototyping is higher than for commercial/bulk quantities.

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## Why this design?



## Conclusion

- The Hive-Stat meets the standards for a 1 MW thermal-solar power plant using the reflected light of the Sun off heliostat surfaces
- The Hive-Stat is a unique and innovative design that accomplishes this, while also addressing the need for a small-scale easily deployable heliostat

