



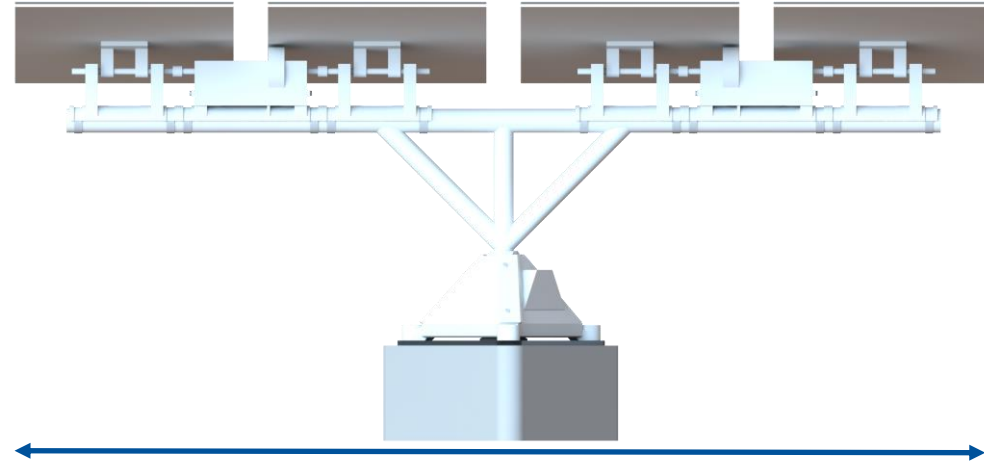
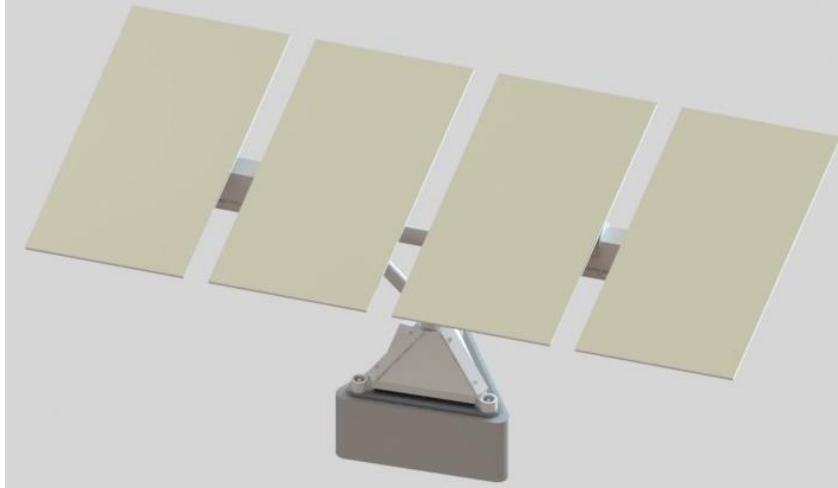
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Azim6 Heliostat

Section 13337, Group 6

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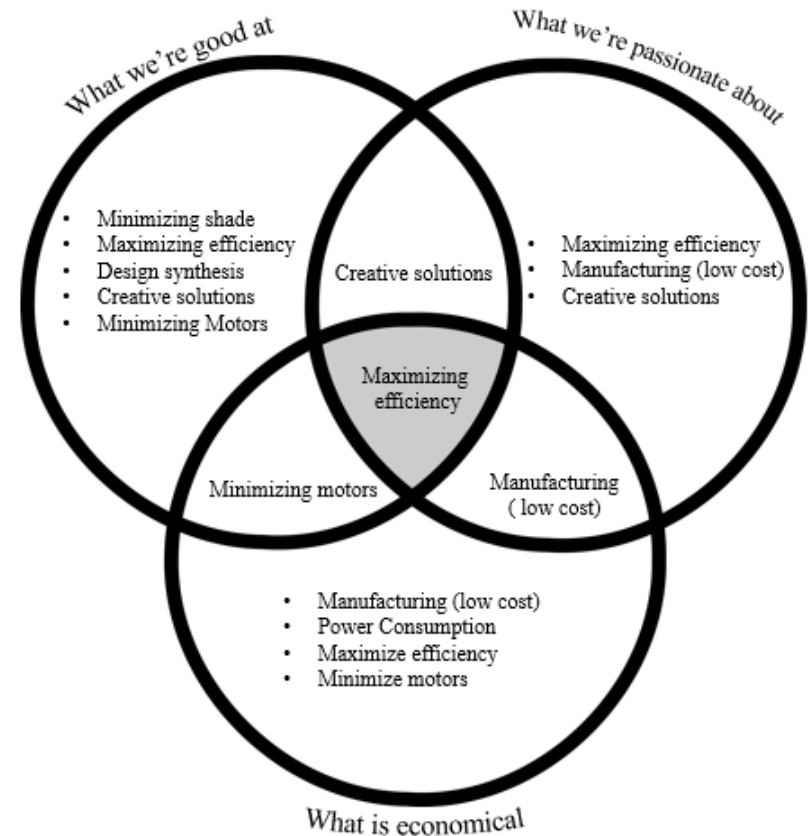
The Azim6 Heliostat

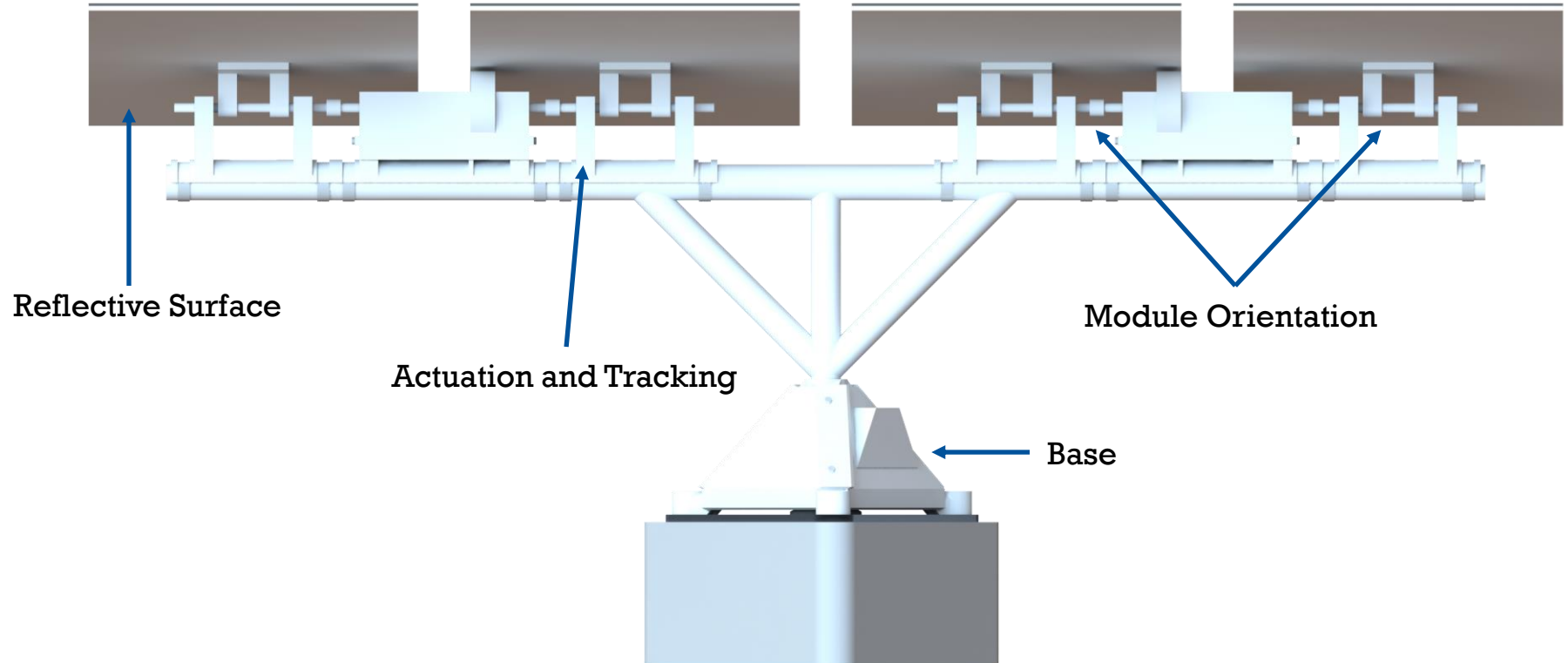


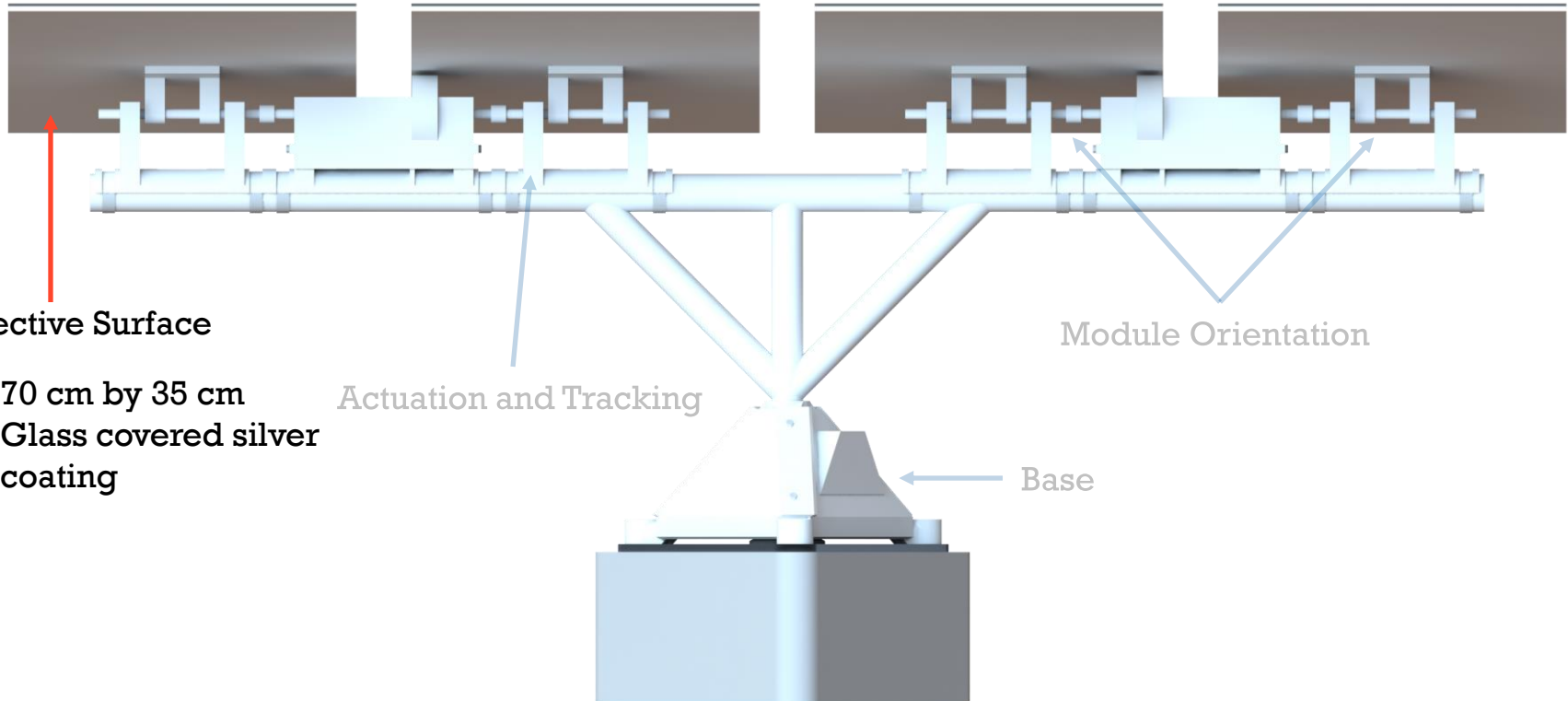
1.87 meters

Guiding Design Principles

- **Maximizing Efficiency:** Added mirror modularity to eliminate downtime.
- **Reducing motor count:** Incorporated a revolving base.
- **Creative Design Solutions:** Single piece inject modeling to reduce parts.
- **Minimizing Manufacturing Processes:** Utilize 3-D printing to eliminate as many machined components as possible.







Reflective Surface

- 70 cm by 35 cm
- Glass covered silver coating

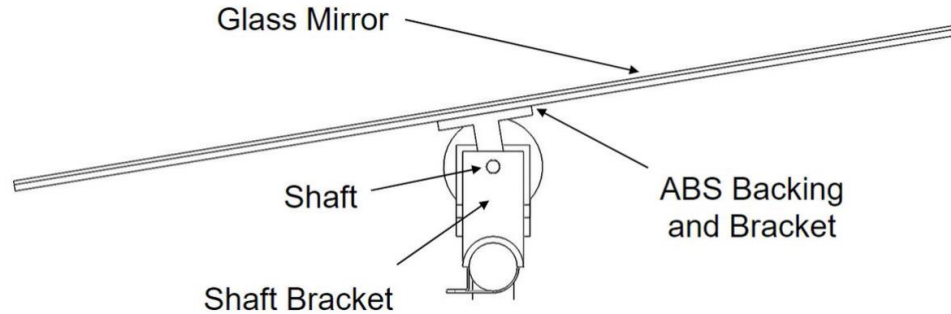
Actuation and Tracking

Module Orientation

Base

Reflective Surface

- 3mm thick glass over silver coating
- Reflectivity of 89-94%
- Coating seal integrity up to 300 ° F
- Supported by ABS backplate



Reflective Surface Analysis

The solar energy collection field made of individual heliostat units must deliver to a central receiving tower target a concentrated focal thermal input power of 1 MW after losses.

$$\blacksquare \dot{Q}_{use} = \dot{Q}_{in} - \dot{Q}_{loss}$$

$$\blacksquare \dot{Q}_{in} = \eta_{optical} \sum_{i=1}^n G_{bt,i} A_i$$

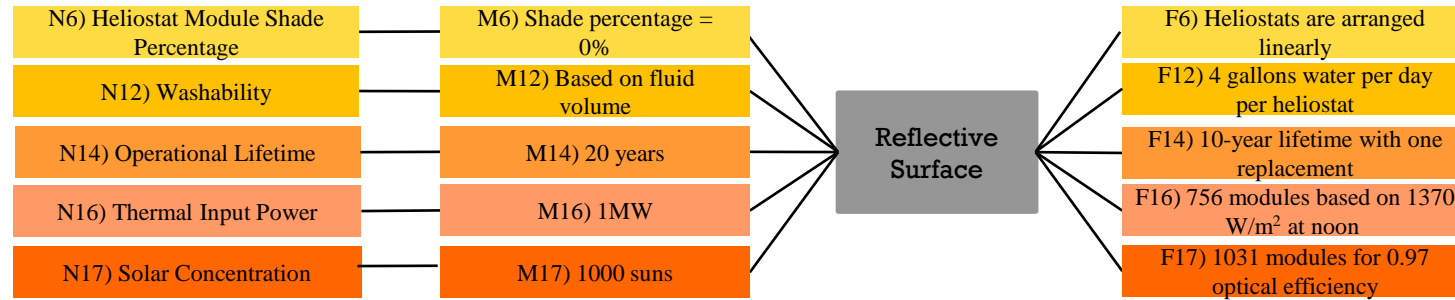
$$\blacksquare \dot{Q}_{loss} = \sigma T_{rec}^4 A_{rec}$$

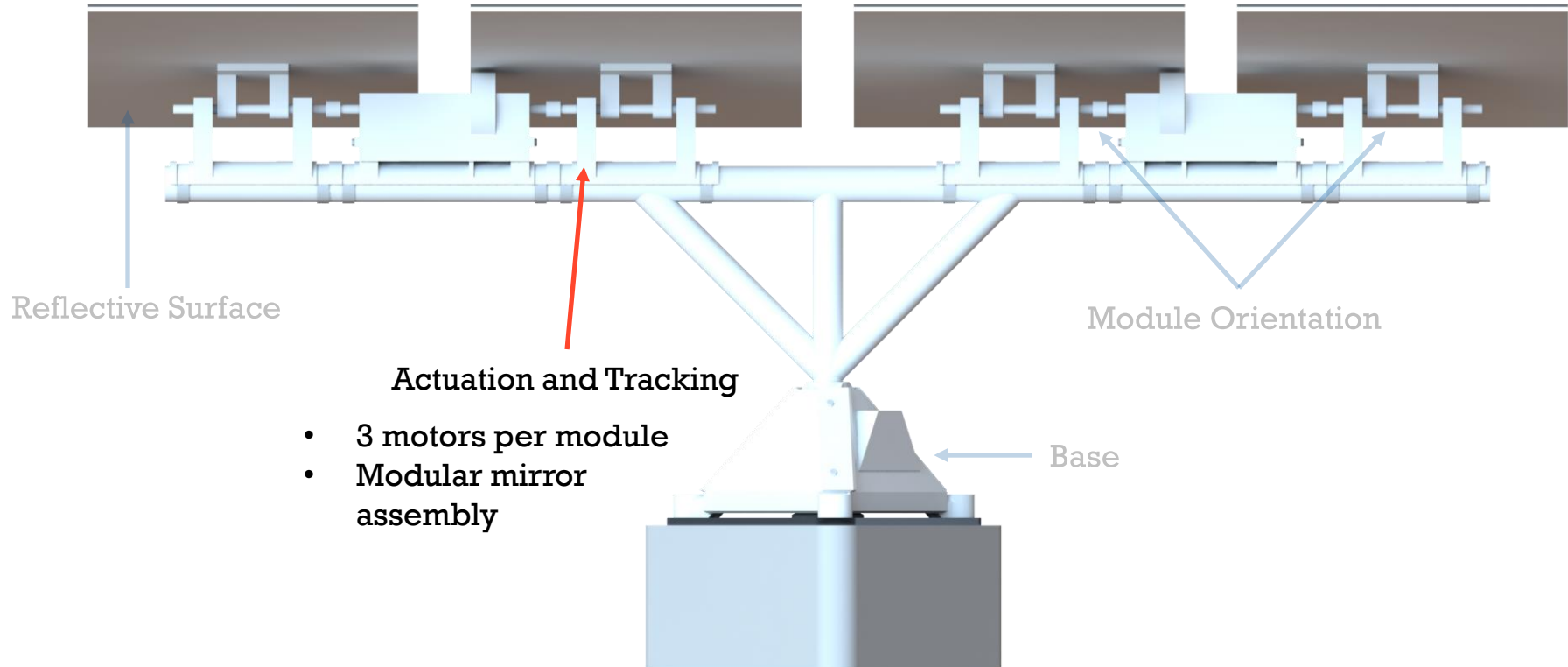
$$\blacksquare CR = \frac{\dot{Q}_{in}}{G_{bt,i}} = \eta_{optical} n A_i$$

- \dot{Q}_{use} : Usable Thermal Input Power
- \dot{Q}_{in} : Thermal Input Power from Heliostat; \dot{Q}_{loss} : Radiative Heat Loss
- $\eta_{optical}$: Optical Efficiency of Material Selected = 0.97
- G_{bt} : Radiative Flux to Earth $\approx 1370 \frac{W}{m^2}$
- A_i : Area of Heliostat = $0.98 m^2$
- A_{rec} : Area of Receiver = $10 m^2$
- A_{rec} : Temp of Receiver, Ambient Temp of Vegas = $47.22 \text{ }^\circ\text{C}$
- σ : Stefan-Boltzmann constant = $5.67 * 10^{-8} \frac{W}{m^2} \cdot K$
- n : Number of Modules in Field = 1000 modules

Analysis Continued

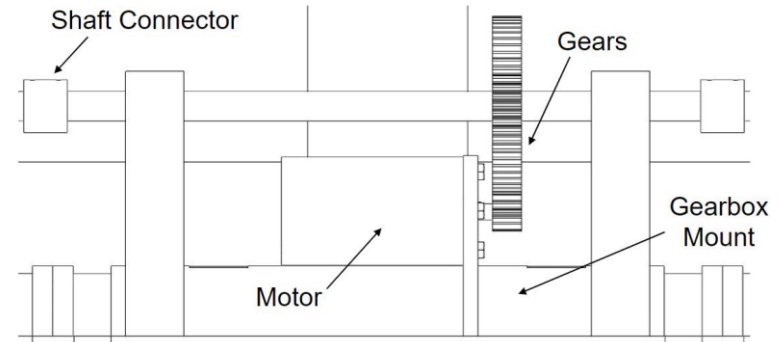
- $\dot{Q}_{in} = 1.433 \text{ MW}$
- $\dot{Q}_{loss} = 5972.97 \text{ W}$
- $\dot{Q}_{use} = 1426581.23 \text{ W} = 1.427 \text{ MW}$
- The usable thermal input power produced is over the requirement of 1 MW
- $CR = 1045.66 \text{ suns}$
- Solar concentration ratio exceeds customer requirement of 1000 suns





Actuation and Tracking

- Single piece drivetrain for mirror control
- Fully modular mirror assembly
- Full module rotation from base motor
- Only 3 motors needed for module tracking
- Shrouding to protect from harsh conditions

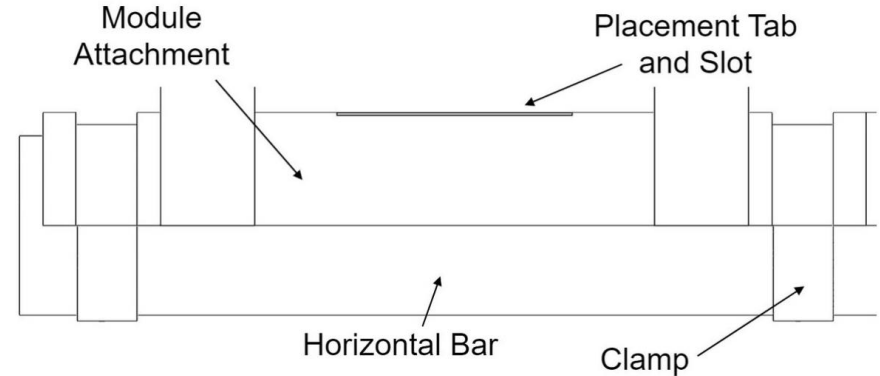


Modularity

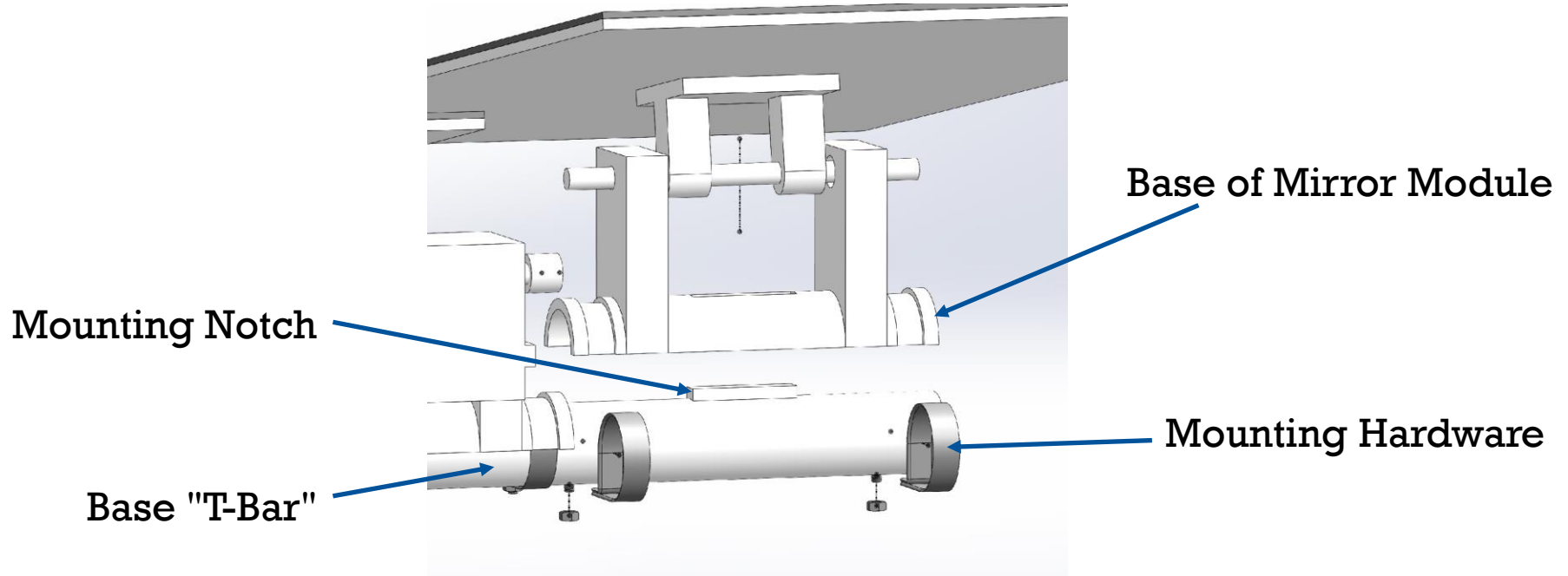
■ Each mirror Assembly contains:

- Mirror and backplate
- Gear
- Driveshaft
- Mounting mechanism

- Allows for easy cleaning and repair without losing operational time



Exploded View of Module



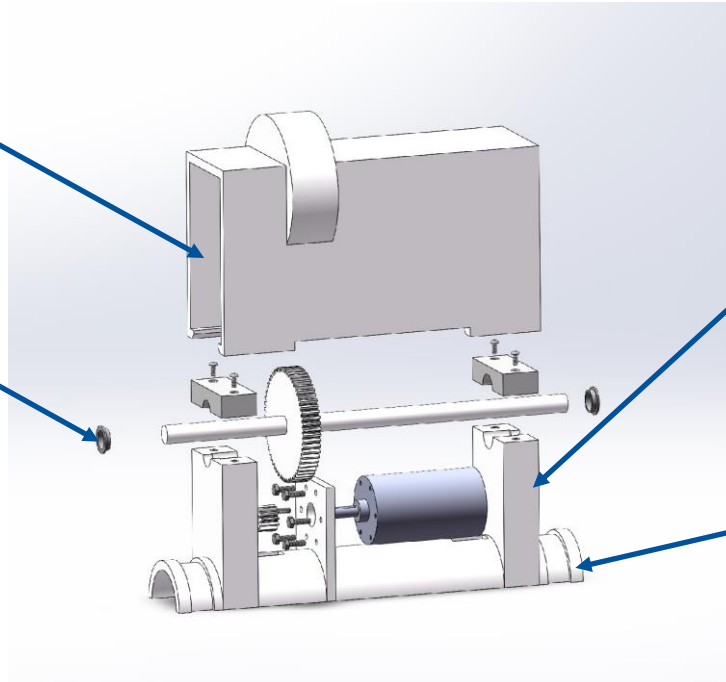
Exploded View of Actuation System

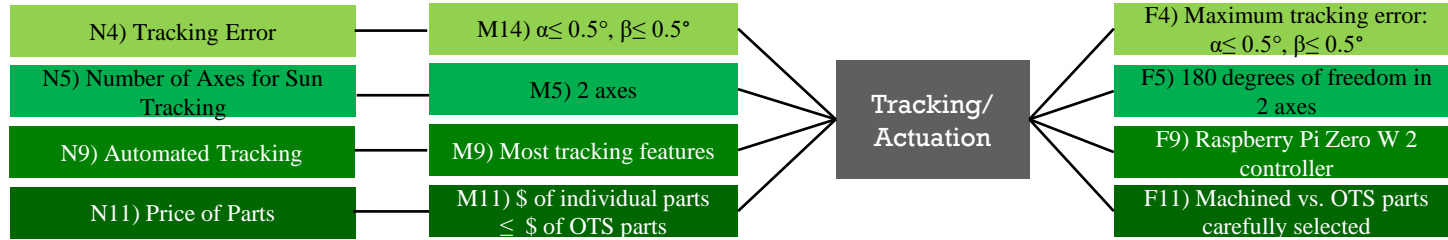
Protective Housing

Shaft Bearing

Shaft Support

Base of Mirror Module





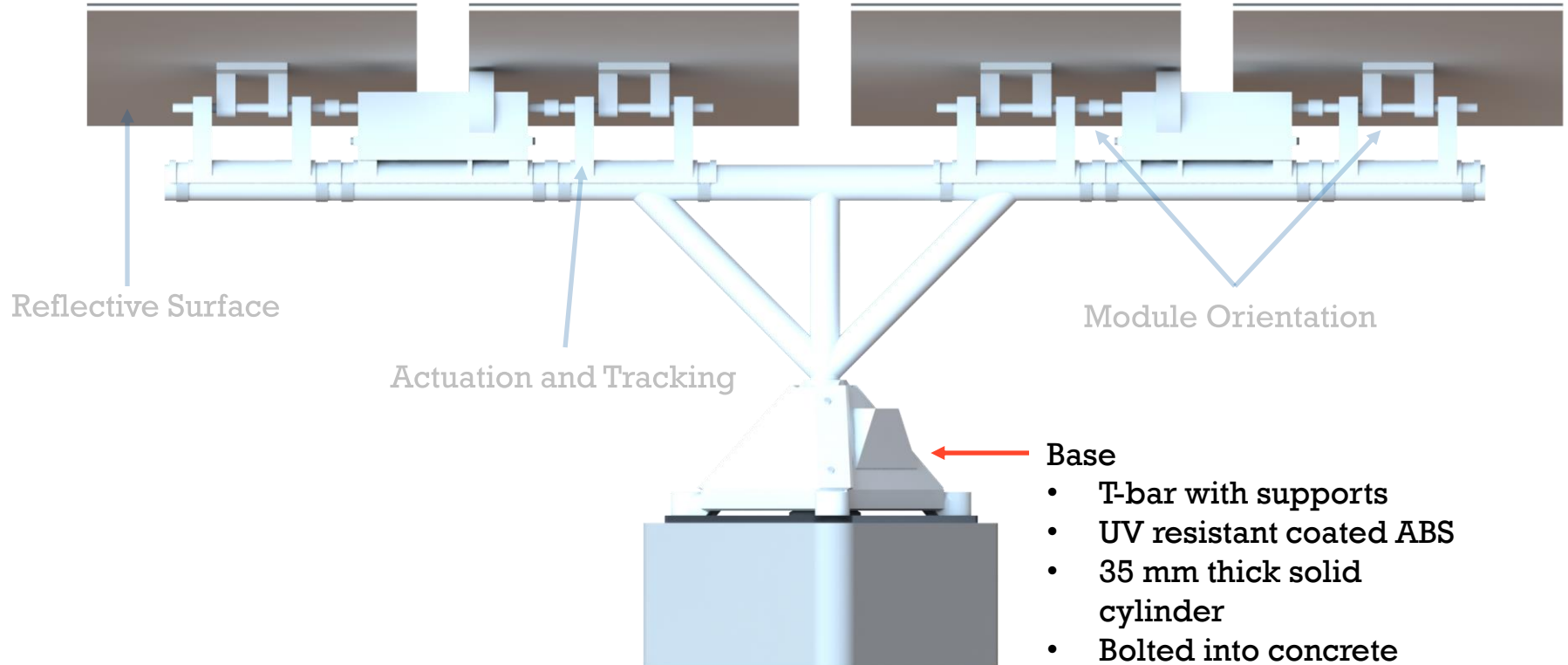
Motors

- All motors are supplying 1.47 Nm torque.
- The mirrors are equipped with a 5:1 gear reduction.
- The base is equipped with a 16.5:1 gear reduction.
- The base is actuated using a belt drive system to obtain its gear ratio.

ABS Covering Heat Transfer Analysis

Assumptions: Opaque Surface : $\rho + \alpha = 1$, Diffused Surface : $\varepsilon = \alpha$

- $\frac{dE_{sy}}{dt} = \dot{Q}_{in} - \dot{Q}_{out} + \dot{W}_{in} - \dot{W}_{out}$
- Steady State: $\frac{dE_{sy}}{dt} = 0$, $\dot{Q}_{out} = \dot{Q}_{in} + \dot{W}_{in}$
- $A_{cover} \varepsilon_{ABS} \sigma (T_{ABS}^4 - T_{surr}^4) = A_{cover} \varepsilon_{sand} \sigma (T_{ABS}^4 - T_{surr}^4) + 4.12W$
- $T_{ABS} = \sqrt[4]{\frac{A_{cover} \varepsilon_{sand} \sigma (T_{ABS}^4 - T_{surr}^4) + 4.12W}{A_{cover} \varepsilon_{ABS} \sigma}} + T_{surr}$
- $T_{ABS} = 79.43 \text{ } ^\circ\text{C}$
- A_{cover} : Surface Area Heat Transfer = 0.0342 m^2
- ε_{sand} : Sand Emissivity = 0.91
- ε_{ABS} : ABS Emissivity = 0.92
- T_{sand} : Sand Temp = $65.65 \text{ } ^\circ\text{C}$
- T_{surr} : Ambient Temp of Vegas = $47 \text{ } ^\circ\text{C}$
- σ : Stefan-Boltzmann constant = $5.67 * 10^{-8} \frac{W}{m^2} \cdot K$



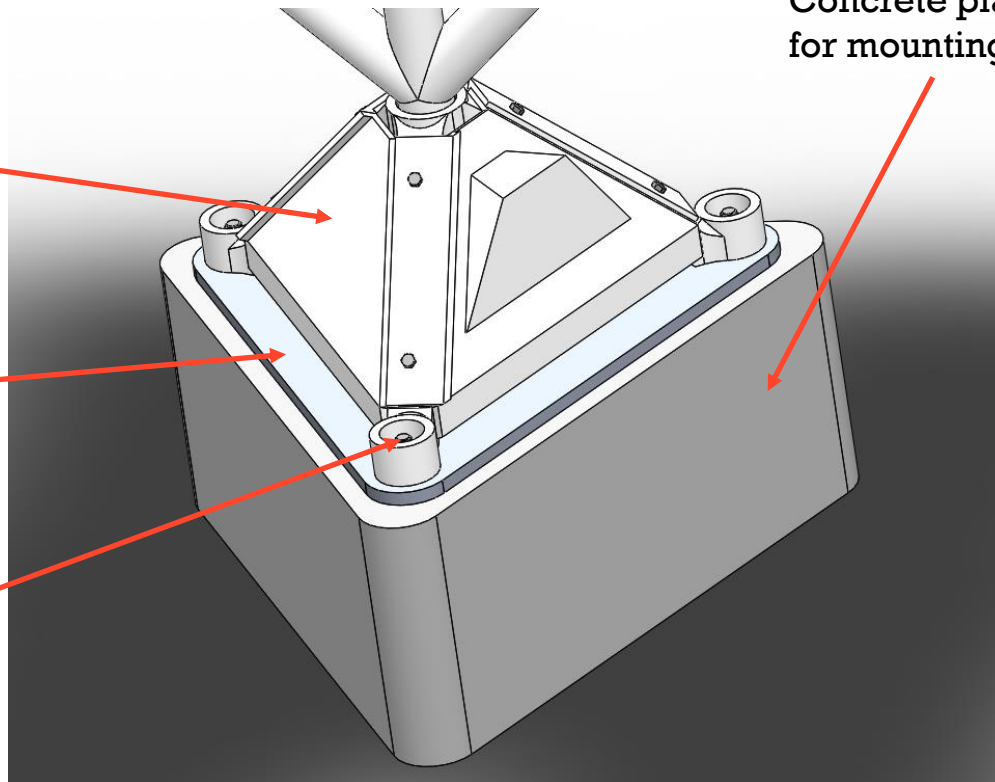
Base Platform

ABS covering,
lightweight, sand-
resistant

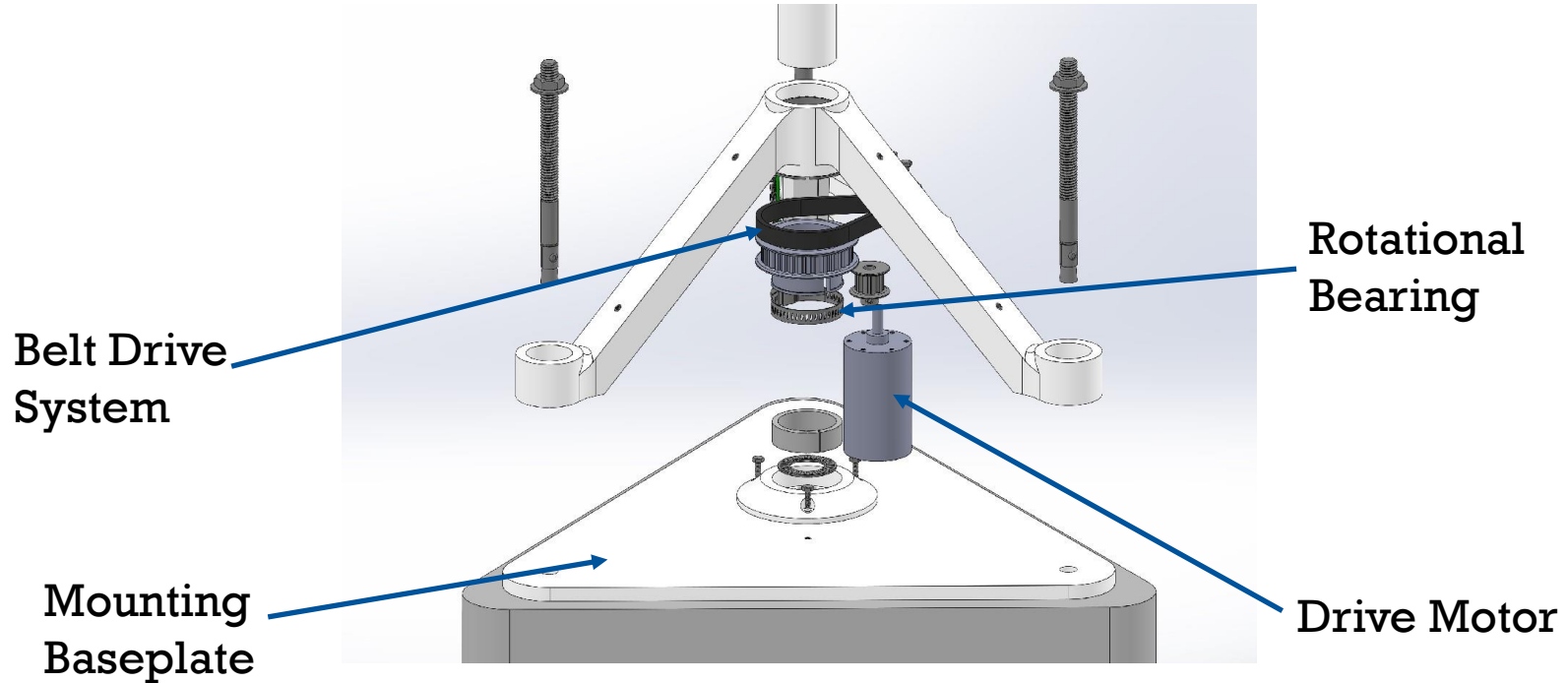
Rounded triangular
base for stability
and aesthetics

3x galvanized
concrete anchors

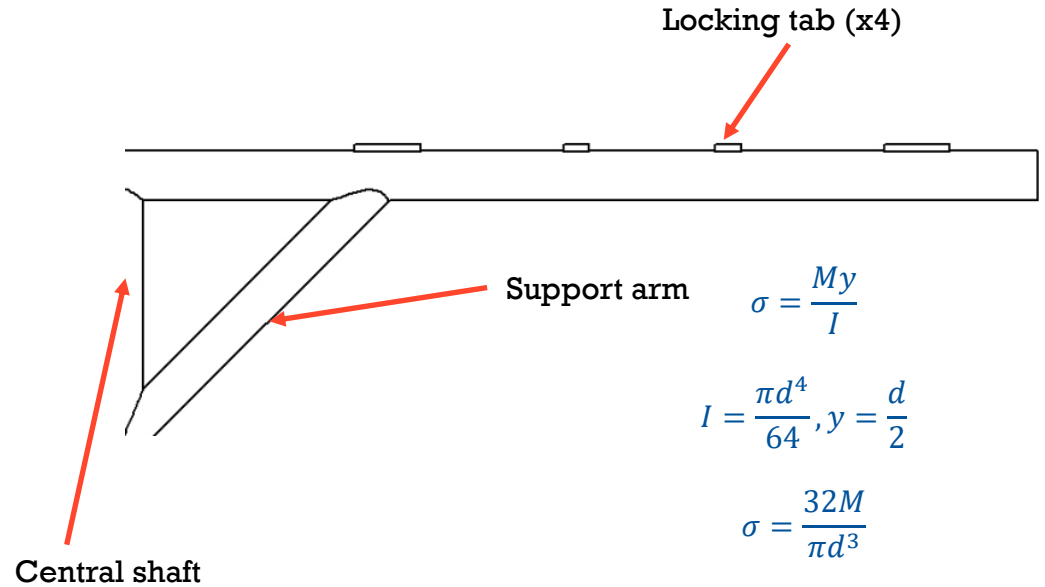
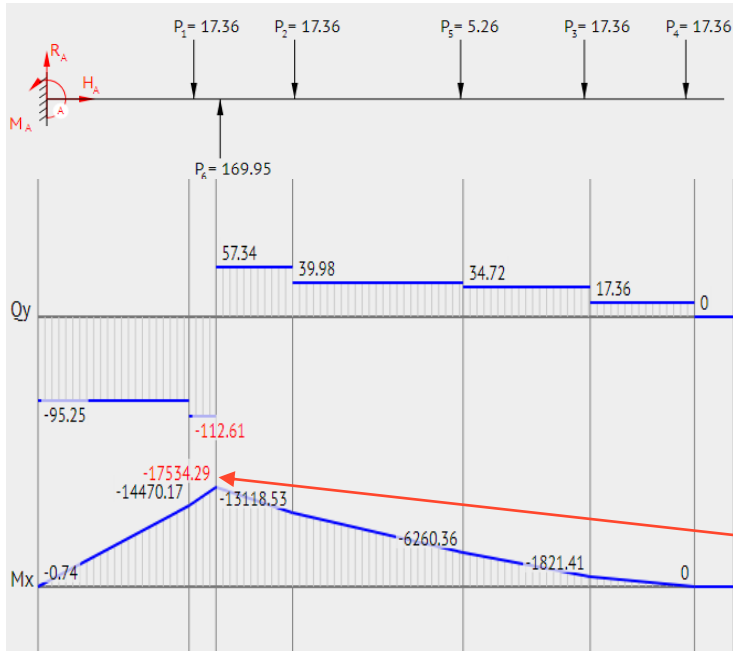
Concrete platform
for mounting



Exploded View of Base



Base



$$\sigma = \frac{My}{I}$$

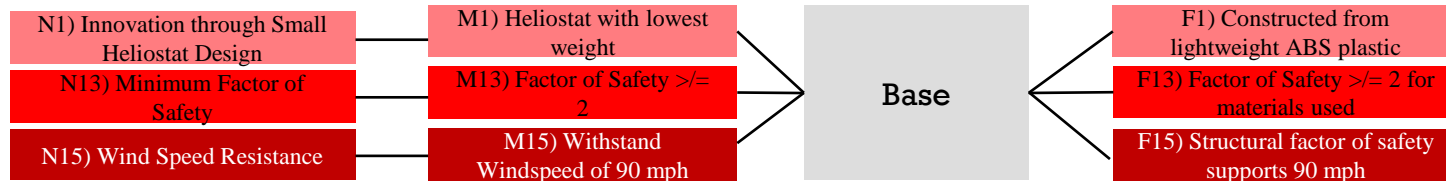
$$I = \frac{\pi d^4}{64}, y = \frac{d}{2}$$

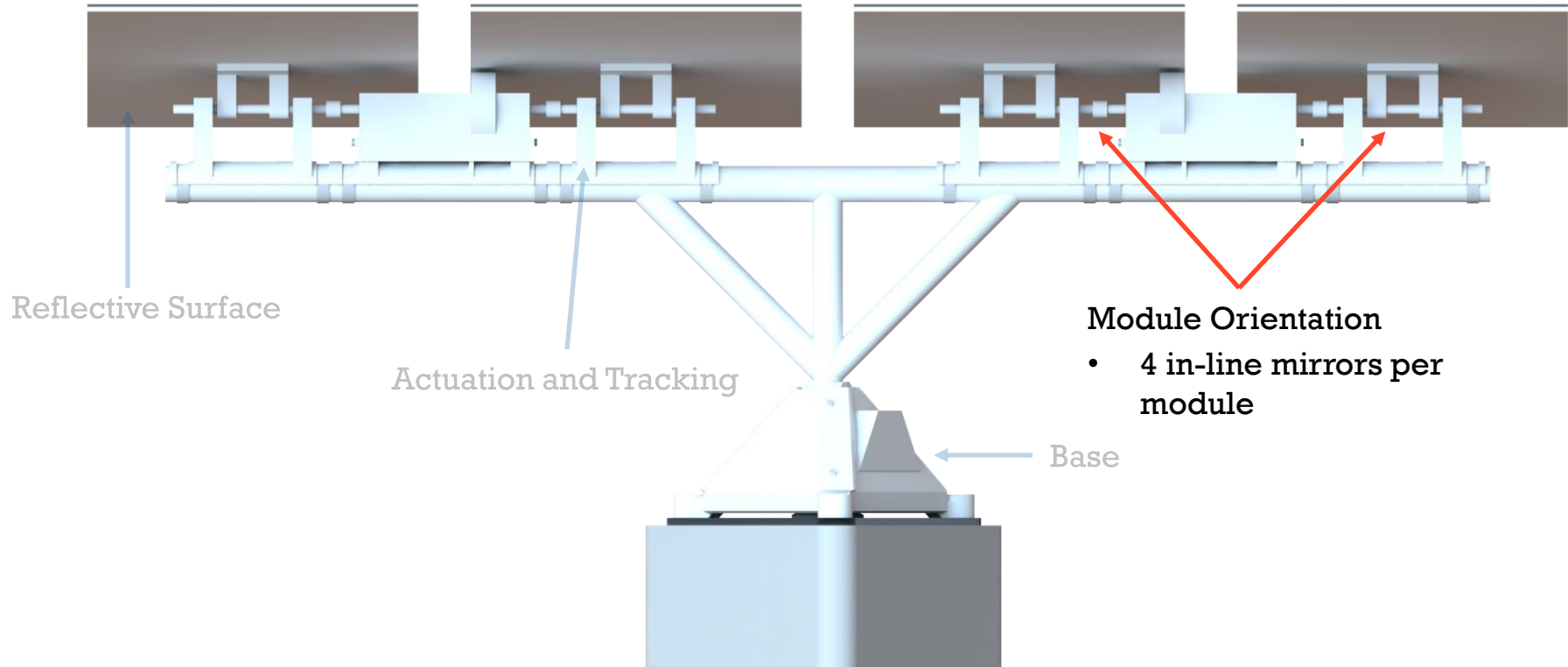
$$\sigma = \frac{32M}{\pi d^3}$$

$$\sigma = 3.25 \text{ MPa}$$

$$n = \frac{\sigma_y}{\sigma} = \frac{13 \text{ MPa}}{3.25 \text{ MPa}} = 4$$

Maximum moment (Nmm)

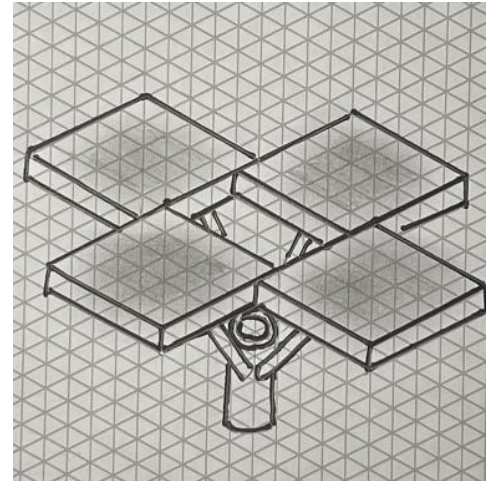
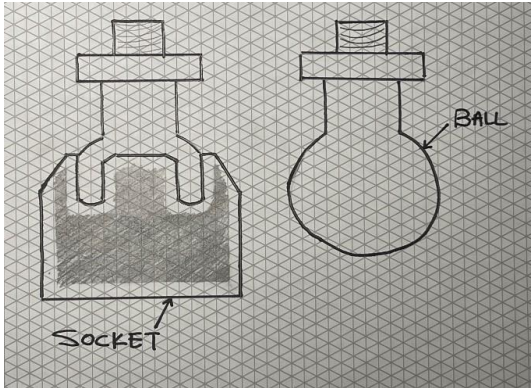


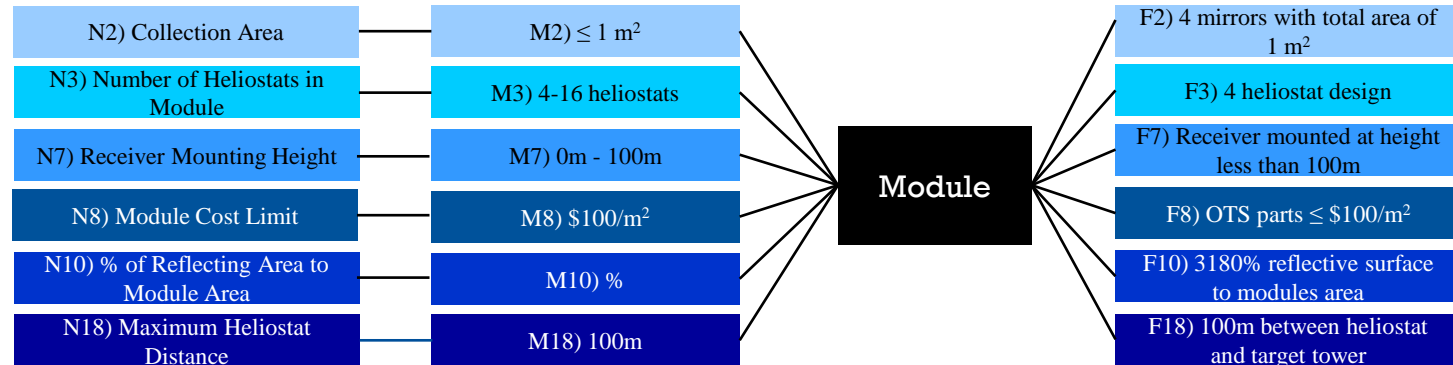


Module Orientation

- Each module has four 0.7 m by 0.35 m mirrors
- Total reflective area of 0.98 m² per module
- Eliminates shading of other mirrors in the module

Where we started...



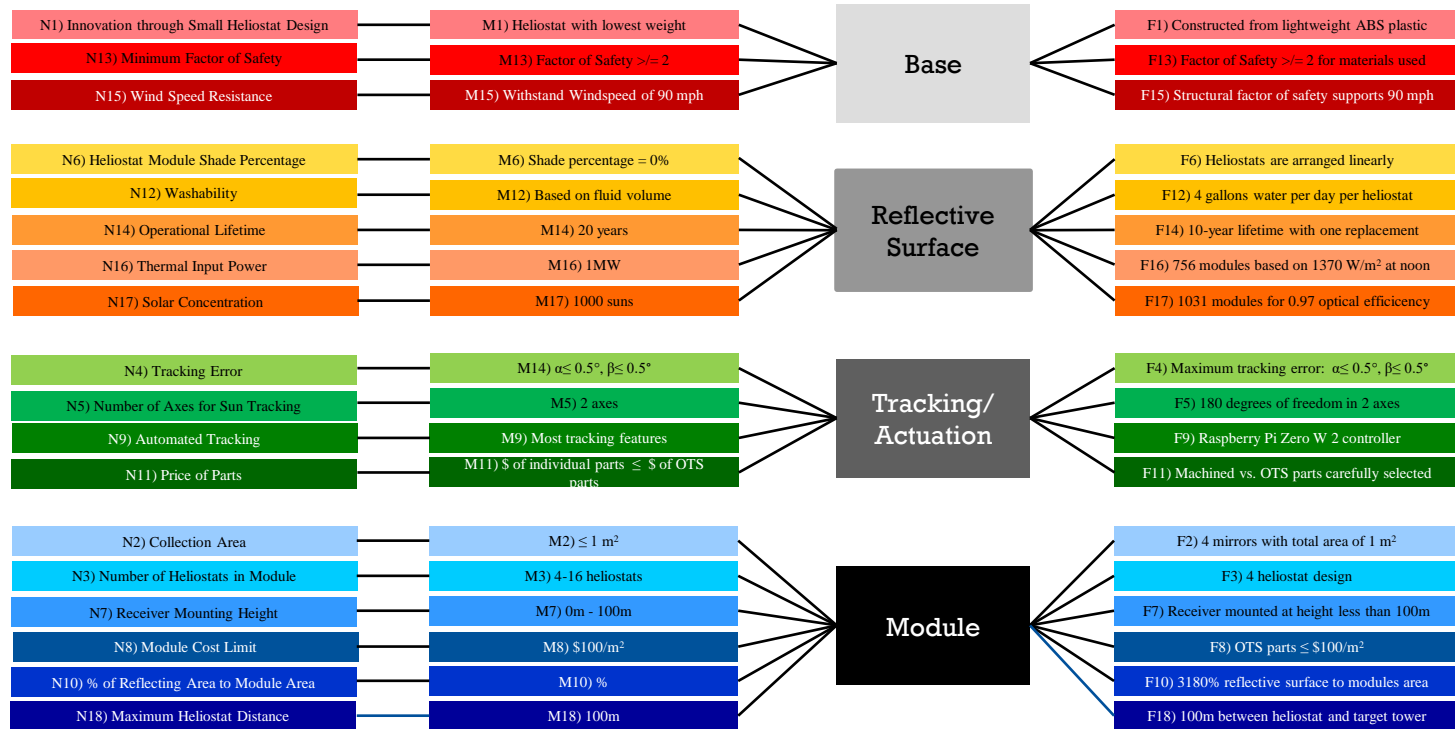


Full Scale Prototype Cost

Cost Breakup	Total Cost
OTS Cost	\$103.57
Raw Material Cost	\$26.40
Manufacturing Labor	\$21.59
Assembly Labor	\$4.38
Energy Consumption	\$0.03
Total Cost	\$155.97

Mass Production Cost

Cost Breakup	Total Cost
OTS Cost	\$77.68
Raw Material Cost	\$18.48
Manufacturing Labor	\$21.59
Assembly Labor	\$4.38
Energy Consumption	\$0.03
Total Cost	\$122.16



Conclusion

Our design:

- Leverages 3-D printing and injection molding to reduce costs
- Incorporates modularity to ensure lifetime needs
- Reduction of motors to reduce cost and part numbers

Thank You

We would like to thank our corporate sponsors, Northrop Grumman, Cummins, Carrier, and Aurigo, for their support for engineering education alongside UF Department of Mechanical and Aerospace engineering.